# RELAYS - HIGH SPEED. <br> $3 / 401 \ldots$ AND $3 / 402 \ldots$ SINGLE CONTACT TYPE. <br> ADJUSTMENTS. 

(Replaces Issue 2, 1954.)

1. INTRODUCTION.
1.1 The adjustments described in this Instruction apply to High Speed Relays types $3 / 401 \ldots$, and $3 / 402 \ldots$, and to the equivalent Siemens (now AEI) types i.e. Nos. 88, 89, 99 and 113.
1.2 The two relay types are almost identical, the only differences are concerned with the coil; 3/401..., has a single coil and $3 / 402 \ldots$, has two coils and a larger tag assembly. Fig. 1 shows the plan view of $3 / 402$; for details refer Drawing CE. 60077 and CE. 60078.
1.3 Relays $3 / 401$ and $3 / 402$ are in general, comparable with the superseded Siemens (ABI) types No. 73 and 85, however the following differences can exist:Relays $3 / 401$ and $3 / 402$.
(i) Are "ourrent" adjusted. (Red Label.)
(ii) Have their coil spools held in position by a clip.
(iii) Have a different tag numbering.
(iv) Have a break contact screw incorporating a ratchet device similar to the tensioning screw.
1.4 Contact material on all these relays may be platinum or platinum-iridium. Platinum contacts are identified by a single notch in the end of the spring whilst platinum-iridium is identified by two notches.


FIG. 1. HIGH SPEED RELAY TYPE 3/402....
Distribution 4, 32, 96.
Page 1.
Issue 1, 1963.

## TELEPHONE

Relays
AD 5001
2. COMMENTS.
2.1 The current values, listed in Appendix 1 and 2, apply when checks or readjustments are being made and this data must be consulted before commencing maintenance. Where Siemens (AEI) adjustment cards are held, these may be used.
2.2 No permanent alterations are to be made to the standard adjustments without first obtaining approval from Headquarters. However, it may be necessary to try out slight modifications to the standard adjustments before submitting a report of the results.
2.3 Adjustments are to be made in accordance with the methods described in the following paragraphs of Section 3 and in that order.
2.4 Where the instructions specify the armature to be electrically operated, the specified saturate current figure is to be used; this figure should not be exceeded.
2.5 The contact screws must be a smooth friction fit in the contact pillars when all adjustments are being made. This is to prevent any loss in adjustment when the contact locking screws are finally tightened.
2.6 Disconnect and remove the relay from its mounting before replacing any worn or damaged parts.
3. STANDARD ADJUSTMENTS.
3.1 Preliminary.
(i) Check that all baseplate-fixing screws are tight.
(ii) Check that the coils are fimmly secured by the fixing clip.
(iii) Check that the tension of the ratchet-spring against the knurled edge of the armature tensioning screw is between 50 to 100 grammes.
(iv) Check that the tension of the ratchet-spring against the knurled edge of the break contact screw is between 50 to 100 grammes. Earlier relays were fitted with a break contact screw without this ratchet.
3.2 Alignment.
(i) Withdraw the tensioning screw until it is clear of the buffer spring.
(ii) Check that the buffer spring rests against the tensioning-screw bracket and that it is clear of the contact spring.
(iii) Check that the buffer spring is aligned with the contact spring so that pressure will be evenly applied across the contact spring. Where a projection is provided at the centre of the buffer spring, this is to bear on the centre of the contact spring.
(iv) Check the contacts to ensure they are not more than one-third of. a contact diameter out of alignment.
(v) Loosen the contact-locking screws and withdraw the make and break contacts clear of the lever spring contacts.
(vi) Check that the contact spring is straight up to the amature and that from there on, there is approximately a $3^{\circ}$ set towards the break contact.
(vii) Check that the armature rests lightly in contact with and parallel to the rear pole face.
(viii) When adjustment is necessary remove the contact spring fixing sorews and use Bent Duckbill Pliers (tool No.211). Re-assemble with the aid of Fine Taper-Nose Pliers (tool No. 220) to hold the components in position. Before tightening the fixing screws check for buffer spring alignment 3.2(iii) and contact alignment 3.2 (iv). The elongated fixing holes enable the necessary movement to be achieved.
3.3 Residual Gap. Set the residual gap ( $2-3 \mathrm{mils}$ ) by reference to the contact clearance (4-5 mils) as described below, unless otherwise specified:-
(i) Relays without the break-contact ratchet adjustment:-
(a) Operate the armature electrically.
(b) Advance the make-contact screw until it just touches the spring contact. This point should be determined electrically by means of the Current-flow Test Set.
(c) Check that the slightest withdrawal of the make-contact disconnects the tester circuit. Leave the contacts just touching.
(d) Insert a 5 -mil feeler gauge between the break-contact and the spring contact, and advance the break-contact, until the gauge is just gripped between the contacts.
(e) Remove the 5-mil gauge and check that a 4-mil gauge passes freely between the contacts.
(f) Release the armature.
(g) Advance the make-contact until it just makes contact with the spring contact. Check as in 3.3(i)(b) and (c).
(h) Tighten the make-contact locking-screw.
(j) Withdraw the break-contact clear of the lever-spring contact.
(ii) Relays with the break-contact ratchet adjustment. Note that one notch on the periphery of the break-contact screw is equivalent to 0.5 mil traverse of the contact.
(a) Operate the armature electrically.
(b) Advance the break-contact until it just touches the spring contact. This point should be determined electrically by means of the Current-flow Test Set.
(c) Check that withdrawal of the break-contact, by one notch, disconnects the tester circuit. Leave the contacts just touching.
(d) Retract the break-contact screw by nine notches.
(e) Release the armature.
(f) Advance the make-contact until it just touches the spring contact.
(g) Check that the slightest withdrawal of the make-contact disconnects the tester circuit. Leave the contacts just touching.
(h) Tighten the make-contact locking screw.
3.4 Contact Opening. Set the contact opening at 4 to 5 mils as described below, unless otherwise specified:-
(i) Relays without the break-contact ratchet adjustment:-
(a) With the armature released, insert a 5-mil feeler gauge between the make-contact and the spring contact.
(b) Advance the break-contact until the gauge is just gripped between the contacts.
(c) Remove the 5 -mil gauge and check that a 4 -mil gauge passes freely between the contacts.
(d) Tighten the break-contact locking-screw.
(e) Check contact opening.
(ii) Relays with the break-contact ratchet adjustment:-
(a) Check that withdrawal of the break-contact, by one notch, disconnects the circuit between the make-contact and the spring contact. Leave the contacts touching.
(b) Retract the break-contact screw by nine notches.
(c) Tighten the break contact locking-screw.
3.5 Break-Contact Pressure. Set the break-contact force at 12 to 24 grammes, to ensure the correct contact pressure, as described below.
(i) Advance the tensioning-screw until the contact spring rests against the break-contact with a pressure that resists 15 grammes and moves with 21 grammes, unless the adjustment data specified a contact force other than 12 to 24 grammes. In the latter case, the contact force should be adjusted towards the mean of the specified values. The contact force should be measured at the centre of the tip of the contact spring. If the $3^{\circ}$ set in the contact spring has been correctly applied the required contact pressure will be obtained without excessive bowing of the lever-spring between the rear pole face and the fixing point of the spring.
3.6 Current Tests. Readjust relays $3 / 401 \ldots$ and $3 / 402 \ldots$, to their readjust values:-
(i) Check the performance of the relay against the current values specified on the relay adjustment data.

Make the current tests in the following order - Saturate; Hold; Release; Non-Operate; and Operate.
(ii) If the current figures are met, the relay adjustment is completed.
(iii) If the current figures are not met, vary the break-contact force, within the limits specified on the relay adjustment data, until the required current conditions are satisfied. If limits of break-contact force are not specified, assume a range of 12 to 24 grammes.
(iv) If the current figures cannot be met within the specified range of break-contact force, re-check the residual gap and contact opening.
(v) If it is not possible to meet the current figures within the specified tolerances, change the relay.
4. TOOLS.
4.1 The following tools are required for adjusting single-contact-unit High-Speed Relays:-

| Tool No. | Description |
| :--- | :--- |
| 139 | Gauge, thickness, $0.0015^{\prime \prime}$ to $0.015^{\prime \prime}$ |
| 154 | Gauge, tension, 4-24 grammes. |
| 152 | Gauge, tension, 50-250 grammes. |
| 211 | Pliers, bent duckbill. |
| 220 | Pliers, fine taper nose. |

4.2 The tools specified must be used only for the purpose for which they are intended. Do not use tools that might cause damage to screws, nuts or springs.


| Relay <br> Code | Coil |  | Current Values (MA) |  |  |  |  |  |  |  |  | Siemens Equivalent |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Code | Resist (Ohms) | Sat. | TEST |  |  |  | RE-ADJUST |  |  |  | $\begin{aligned} & \text { Early } \\ & \text { Type } \end{aligned}$ | Improved Type |  |
|  |  |  |  | Hold | Rel. | $\begin{gathered} \text { Non- } \\ \text { Op. } \end{gathered}$ | Op. | Hold | Fel. | $\begin{array}{\|l\|} \hline \text { Non- } \\ \text { Op. } \\ \hline \end{array}$ | Op. |  |  |  |
| $3 / 401 \mathrm{~T}$ | 23/5c0/479 | 1,600 | 29 |  | 4.2 | 5.7 | 9.5 |  | 4.5 | 6.0 | 9.0 |  | 88AG |  |
| 3/401U | 1/Sco/479 | 145 | 90 |  | 11.5 |  | 27 |  | 12 |  | 26 |  | 88AJ |  |
| $3 / 401 \mathrm{~V}$ | 24/5c0/479 | 15 | 270 |  |  | 57 | 74 |  |  | 60 | 70 |  | 88AE |  |
| 3/401w | 25/5co/479 | 210 | 70 |  | 7.6 | 16 | 23 |  | 8 | 17 | 22 |  | 88AK | Max. Contact Force 30 gms . |
| 3/401X | 26/Sco/479 | 40 | 188 |  |  | 36 | 46 |  |  | 38 | 44 |  | 88AL |  |
| $3 / 401 \mathrm{Y}$ | 7/5co/479 | 50 | 140 |  |  | 26.5 | 33 |  |  | 28 | 31.5 |  | 88AU |  |
| 3/4012 | 6/5co/479 | 75 | 120 |  | 18 |  | 40 |  | 19 |  | 38 |  |  |  |
| $3 / 401 \mathrm{AA}$ | 14/5c0/479 | 11 | 300 |  | 40 |  | 87 |  | 42 |  | 84 |  | 88AT |  |
| 3/401AC | 28/5c0/479 | 5.5 | 460 |  | 46 | 88 | 131 |  | 49 | 93 | 125 |  | 88AX |  |
| $3 / 401 \mathrm{AE}$ | 10/5C0/479 | 800 | 41 | 6.0 | $4 \cdot 4$ |  | 9.6 | 5.7 | 4.6 |  | 9.1 |  | 88AM | Adjust Break Contact Pressure to meet current Figures. |
| $3 / 401 \mathrm{AF}$ | 12/SCO/479 | 1,700 | 27 |  |  | 7.1 | 8.8 |  |  | 7.4 | 8.3 |  |  |  |
| 3/401AG | 31/5co/479 | 5.5 | 410 | 92 | 40 |  | 115 | 88 | 42 |  | 109 |  |  |  |
| 3/401AH | 24/SC0/479 | 15 | 270 |  | 40 |  | 89 |  | 42 |  | 84 |  | 88AP | Max. Contact Force 30 gms. |
| 3/401A.J | 32/SC0/479 | 200 | 100 |  | 11.1 |  | 27.8 |  | 11.6 |  | 26.4 |  |  |  |
| $3 / 401 \mathrm{AAA}$ | 10/SCO/479 | 800 | 41 | 10 |  | 7.1 | 13 | 9.5 |  | 7.5 | 12 |  |  | Adjust Break <br> Contact Pressure <br> to meet current <br> Figures. |



REAR VIEW OF TAG ALLOCATION

| Relay Code | Coil |  |  | Current Vailues (MA) |  |  |  |  |  |  |  |  |  | Siemens Equivalent |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. | Code | Resist <br> (Ohms) | Coil | Sat. | TEST |  |  |  | PE-ADJUST |  |  |  | $\begin{aligned} & \text { Early } \\ & \text { Type } \end{aligned}$ | Improved Type |  |
|  |  |  |  |  |  | Hold | Rel. | $\begin{gathered} \hline \text { Non- } \\ \text { Op. } \\ \hline \end{gathered}$ | Op. | Hold | Rel. | $\begin{aligned} & \hline \text { Non- } \\ & \text { Op. } \end{aligned}$ | Op. |  |  |  |
| 3/402A | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $11 / 5 C 0 / 479$ $11 / 5 C 0 / 479$ | 260 260 | $1+2$ | 33 |  | 3.8 |  | 12 |  | 4.0 |  | 11 | 85A | 89A |  |
| $3 / 402 \mathrm{~B}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 5 / \mathrm{SCO} / 479 \\ & 5 / \mathrm{SCO} / 479 \end{aligned}$ | 500 500 |  |  |  |  |  |  |  |  |  |  | 85B | 89B | Superseded by 3/402G |
| 3/402C | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 2 / \mathrm{SCO} / 479 \\ & 2 / \mathrm{SCO} / 479 \end{aligned}$ | $\begin{aligned} & 1,000 \\ & 1,000 \end{aligned}$ | $1+2$ | 24 |  |  | 4.7 | 8.0 |  |  | 5.0 | 7.5 | 850 | 890 |  |
| 3/402D | $1$ | $\begin{array}{r} 15 / \mathrm{sco} / 479 \\ 7 / 5 C 0 / 479 \end{array}$ | 50 50 | $\begin{aligned} & 1 \\ & 1 / / 2 \end{aligned}$ | $\begin{aligned} & 170 \\ & 150 \end{aligned}$ | 36 |  | 38 | 51 | 34 |  | 40 | 48 | 85D | 89D |  |
| 3/402E | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 15 / \mathrm{sco} / 479 \\ & 12 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{array}{r} 50 \\ 1,700 \end{array}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 170 \\ 27 \end{array}$ |  |  | 38 | $\begin{aligned} & 51 \\ & 10 \end{aligned}$ |  |  | 40 | $\begin{array}{r} 48 \\ 9.5 \end{array}$ | 85E | 89E |  |
| 3/402F | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 16 / \mathrm{sco} / 479 \\ & 16 / \mathrm{SCO} / 479 \end{aligned}$ | $\begin{aligned} & 850 \\ & 850 \end{aligned}$ | $1+2$ | 19 |  | 2.4 |  | 6.8 |  | 2.5 |  | 6.5 | 85F | 89F |  |
| 3/4026 | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 5 / \mathrm{sco} / 479 \\ & 5 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 500 \\ & 500 \end{aligned}$ | $1+2$ | 24 |  | 2.8 |  | 8.5 |  | 3.0 |  | 8.0 | 85 c | 890 | Supersedes <br> $3 / 402 B$ |
| 3/402H | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 3 / \mathrm{sco} / 479 \\ & 3 / \mathrm{SCO} / 479 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | 1+2 | 50 |  | 5.2 |  | 17 |  | 5.5 |  | 16 | 85H | 89H |  |
| 3/402J | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 1 / \mathrm{SCO} / 479 \\ & 5 / \mathrm{SCO} / 479 \end{aligned}$ | 145 500 |  |  |  |  |  |  |  |  |  |  | 85 J | 89J | Superseded by 3/402P |
| 3/402K | $\begin{aligned} & 4 \\ & 2 \end{aligned}$ | $\begin{aligned} & 7 / \mathrm{Sco} / 479 \\ & 7 / \mathrm{sco} / 479 \end{aligned}$ | 50 | $\begin{aligned} & 1 \\ & 1+2 \end{aligned}$ | $\begin{array}{r} 140 \\ 70 \end{array}$ | 36 | 7.5 |  | 20 | 34 | 8.0 |  | 19 | 85K | 89K |  |
| 3/402L | 2 | $\begin{aligned} & 12 / \mathrm{SCO} / 479 \\ & 12 / \mathrm{SCO} / 479 \end{aligned}$ | $\begin{aligned} & 1,700 \\ & 1,700 \end{aligned}$ | $\begin{aligned} & 1+2 \\ & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 14 \\ & 27 \\ & 27 \end{aligned}$ |  | $\begin{aligned} & 1.4 \\ & 2.8 \\ & 2.8 \end{aligned}$ |  | $\begin{aligned} & 4.5 \\ & 8.1 \\ & 9.7 \end{aligned}$ |  | $\begin{aligned} & 1.5 \\ & 3.0 \\ & 3.0 \end{aligned}$ |  | $\begin{aligned} & 4.3 \\ & 7.7 \\ & 9.2 \end{aligned}$ | 851 | 895 |  |
| 3/402m | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 14 / \mathrm{sco} / 479 \\ & 10 / 5 C 0 / 479 \end{aligned}$ | 11 800 | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 300 \\ 41 \end{array}$ |  | 33 |  | 84 14 |  | 35 |  | $\begin{aligned} & 80 \\ & 13 \end{aligned}$ | 85M | 89M |  |
| 3/402N | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 8 / \mathrm{Sco} / 479 \\ & 3 / \mathrm{sco} / 479 \end{aligned}$ | 1.8 100 | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 820 \\ & 100 \end{aligned}$ |  |  | 190 | $\begin{array}{r} 240 \\ 36 \end{array}$ |  |  | 200 | 230 34 |  | 89AK |  |
| 3/402P | 1 | $\begin{aligned} & 1 / \mathrm{SCO} / 479 \\ & 5 / \mathrm{SCO} / 479 \end{aligned}$ | 145 500 | 1 2 | 90 48 | 13 | 11 |  | 29 18 | 12 | 12 |  | 27 17 |  | 89CL | Supersedes 3/402J |

TELEPHONE
Relays
AD 5001

| Relay Code | Coil |  |  | Current Values (MA) |  |  |  |  |  |  |  |  |  | Siemens Equivalent |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. | Code | Resist (Ohms) | Coil | Sat. | TEST |  |  |  | RE-ADJUST |  |  |  | $\begin{aligned} & \text { Early } \\ & \text { Type } \end{aligned}$ | $\begin{gathered} \text { Improved } \\ \text { Type } \end{gathered}$ |  |
|  |  |  |  |  |  | Hold | Rel. | $\begin{array}{\|l\|} \hline \text { Non- } \\ \text { Op. } \\ \hline \end{array}$ | Op. | Hold | Rel. | $\begin{aligned} & \hline \text { Non- } \\ & \text { Op. } \end{aligned}$ | Op. |  |  |  |
| 3/402Q | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $7 / 5 c 0 / 479$ $7 / 5 c 0 / 479$ | 50 50 |  |  |  |  |  |  |  |  |  |  |  |  | Superseded by 3/402V |
| 3/402R | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 20 / 5 c 0 / 479 \\ 2 / 5 c 0 / 479 \end{array}$ | $\begin{array}{r} 7 \\ 1,000 \end{array}$ | 1 | $\begin{array}{r} 420 \\ 41 \end{array}$ |  |  | 95 | $\begin{array}{r} 130 \\ 17 \end{array}$ |  |  | 100 | $\begin{array}{r} 120 \\ 16 \end{array}$ |  | 89BE |  |
| 3/402S | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 20 / \mathrm{sco} / 479 \\ & 13 / \mathrm{SCO} / 479 \end{aligned}$ | 7  <br> 3  | $\left\lvert\, \begin{array}{l\|l} 1 \\ 2 \end{array}\right.$ | $\begin{aligned} & 420 \\ & 550 \end{aligned}$ | 160 |  | 102 | $\begin{aligned} & 125 \\ & 210 \end{aligned}$ | 150 |  | 107 | $\begin{aligned} & 119 \\ & 200 \end{aligned}$ | 85 X | 89X |  |
| 3/402T | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 19 / 5 c 0 / 479 \\ & 18 / 5 c 0 / 479 \end{aligned}$ | $\begin{array}{r} 7 \\ 120 \end{array}$ | $\begin{aligned} & 1 \\ & 1+2 \end{aligned}$ | $\begin{array}{r} 460 \\ 88 \end{array}$ | 63 | 48 | 15 | 28 | 60 | 50 | 16 | 26 |  | 89BH | Contact Force 12-17 gms. |
| 3/402U | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 5 / \mathrm{sco} / 479 \\ & 5 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 500 \\ & 500 \end{aligned}$ | $1 \begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 48 \\ & 48 \end{aligned}$ |  | 6.2 |  | $\begin{aligned} & 15 \\ & 18 \end{aligned}$ |  | 6.5 |  | $\begin{aligned} & 14 \\ & 17 \end{aligned}$ |  | 89BG |  |
| 3/402V | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 7 / \mathrm{Sco} / 479 \\ & 7 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $1+2$ | 69 | 19 |  | 14 | 23 | 18 |  | 15 | 22 |  | 89BD | Supersedes <br> 3/402Q |
| 3/402W | $\left\lvert\, \begin{aligned} & 1 \\ & 2 \end{aligned}\right.$ | $\begin{aligned} & 22 / \mathrm{SCO} / 479 \\ & 12 / \mathrm{SCO} / 479 \end{aligned}$ | $\begin{array}{r} 26 \\ 1,700 \end{array}$ | $\sqrt{1} \begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{array}{r} 210 \\ 27 \end{array}$ |  |  | 38 | 63 | 7.0 |  | 40 | 60 |  | 89BS |  |
| 3/402X | $\begin{array}{\|l\|l} 1 \\ 2 \end{array}$ | $\begin{aligned} & 22 / 5 C 0 / 479 \\ & 22 / 5 C 0 / 479 \end{aligned}$ | $\begin{aligned} & 26 \\ & 26 \\ & \hline \end{aligned}$ | 1 2 | $\left\lvert\, \begin{aligned} & 210 \\ & 210 \end{aligned}\right.$ |  |  | 50 | $\begin{aligned} & 62 \\ & 75 \end{aligned}$ |  |  | 53 | $\begin{aligned} & 59 \\ & 71 \end{aligned}$ |  | 898N |  |
| 3/402Y | $\begin{array}{l\|l} 1 \\ 2 \end{array}$ | $\begin{aligned} & 12 / \mathrm{sco} / 479 \\ & 21 / \mathrm{sco} / 479 \end{aligned}$ | 1,700 330 | 1 2 | $\begin{aligned} & 27 \\ & 55 \end{aligned}$ | 16 | 2.9 |  | 8.1 | 15 | 3.1 |  | 7.7 |  |  |  |
| 3/4022 | $\begin{array}{l\|l} 1 \\ 2 \end{array}$ | 6/Sco/479 <br> 6/5C0/479 | $\begin{aligned} & 75 \\ & 75 \end{aligned}$ | $1 / / 2$ | 130 |  | 15 |  | 38 |  | 16 |  | 36 |  | 89BY |  |
| 3/402AA | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 1 / \mathrm{Sco} / 479 \\ 16 / 5 C 0 / 479 \end{array}$ | 145 850 | $\left\lvert\, \begin{aligned} & 1 \\ & 2 \end{aligned}\right.$ | $\begin{aligned} & 90 \\ & 38 \end{aligned}$ |  | 11.5 |  | $\begin{gathered} 27 \\ 14 \end{gathered}$ |  | 12 |  | $\begin{aligned} & 26 \\ & 13 \end{aligned}$ |  |  |  |
| 3/402AB | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 22 / 5 C 0 / 479 \\ & 22 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 26 \\ & 26 \end{aligned}$ | $1+2$ | 120 |  | 12 | 23 | 33 |  | 13 | 24 | 31 |  | 89AE |  |
| 3/402AC | $\left\lvert\, \begin{aligned} & 1 \\ & 2 \end{aligned}\right.$ | $\begin{aligned} & 24 / 500 / 479 \\ & 24 / 500 / 479 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | 1+2 | 130 |  |  | 38 | 40 |  |  | 34 | 38 |  | 89 BA |  |
| 3/402AD | $\left\lvert\, \begin{aligned} & 1 \\ & 2 \end{aligned}\right.$ | $\begin{aligned} & 7 / \mathrm{Sc} 0 / 479 \\ & 7 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $1+2$ | 69 |  | 11.5 |  | 25 |  | 12 |  | 24 |  | 89CD | Max. Contact Force 30 gms . |
| 3/402AE | $\left\lvert\, \begin{aligned} & 1 \\ & 2 \end{aligned}\right.$ | $\begin{aligned} & 5 / \mathrm{sco} / 479 \\ & 5 / \mathrm{sco} / 479 \end{aligned}$ | 500 | $\begin{array}{\|l} 1 \\ 2 \end{array}$ | $\begin{aligned} & 48 \\ & 48 \end{aligned}$ |  | 5.7 | 11.0 | $\begin{array}{r} 13.5 \\ 17 \end{array}$ |  | 6 | 11.5 | $\begin{aligned} & 13 \\ & 16 \end{aligned}$ |  | 8942 |  |
| 3/402AF | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 12 / \mathrm{SCO} / 479 \\ & 12 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 1,700 \\ & 1,700 \end{aligned}$ | 1+2 | 14 |  | 2.3 | 3.5 | 5.2 |  | 2.4 | 3.7 | 4.9 |  | 890. | Max. Contact Force 30 gms . |
| 3/402AG | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 3 / \mathrm{ScO} / 479 \\ 24 / \mathrm{SCO} / 479 \end{array}$ | 100 15 | 1 2 | $\begin{aligned} & 100 \\ & 270 \end{aligned}$ |  | 11 |  | $\begin{aligned} & 28 \\ & 90 \end{aligned}$ |  | 12 |  | 27 85 |  | 89BJ |  |
| 3/402AH | $2$ | $\begin{array}{r} 1 / \mathrm{SCO} / 479 \\ 12 / \mathrm{SCO} / 479 \end{array}$ | $\begin{array}{r} 145 \\ 1,700 \end{array}$ | 1 2 | $\begin{aligned} & 90 \\ & 27 \end{aligned}$ |  | 9.5 |  | $\begin{aligned} & 26 \\ & 10 \end{aligned}$ |  | 10 |  | $\begin{array}{r} 25 \\ 9.5 \end{array}$ |  | 899 |  |
| 3/402AJ | 1 | $\begin{aligned} & \hline 27 / \mathrm{sco} / 479 \\ & 17 / \mathrm{sco} / 479 \end{aligned}$ | 15 | 1 | $330$ |  | 47 | 105 | $\begin{array}{r} 131 \\ 79 \end{array}$ |  | 50 | 110 | $\begin{array}{r} 125 \\ 75 \end{array}$ |  | 898X |  |


| Relay <br> Code | Coil |  |  | Current Values (MA) |  |  |  |  |  |  |  |  |  | Siemens Equivalent |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. | Code | Resist (Ohms) | Coil | Sat. | TEST |  |  |  | RE-ADJUST |  |  |  | $\begin{aligned} & \text { Early } \\ & \text { Type } \end{aligned}$ | Improved Type |  |
|  |  |  |  |  |  | Hold | Rel. | Non- <br> Op. | Op. | Hold | Rel. | $\begin{aligned} & \text { Non- } \\ & \text { Op. } \end{aligned}$ | Op. |  |  |  |
| 3/402AK | $2$ | $1 / 5 c 0 / 479$ $1 / 5 c 0 / 479$ | 145 | 1 2 | 90 90 |  |  | 19 21 | 24 30 |  |  | 20 22 | 23 29 |  |  |  |
| 3/402AL | $2$ | $\begin{aligned} & 26 / 500 / 479 \\ & 12 / 500 / 479 \end{aligned}$ | $\begin{array}{r} 40 \\ 1,700 \end{array}$ | $\begin{array}{l\|} 1 \\ 1+2 \end{array}$ | $\begin{array}{r} 190 \\ 26 \end{array}$ | 44 | 4.3 |  | 10 | 42 | 4.6 |  | 9.5 |  | 8902 | Max. Contact Force 30 gms . |
| 3/402AN | 2 | $\begin{array}{r} 7 / 500 / 479 \\ 29 / 500 / 479 \end{array}$ | 50 | $\left\lvert\, \begin{aligned} & 1 \\ & 1+2 \end{aligned}\right.$ | $\begin{array}{r} 140 \\ 41 \end{array}$ | 20 | 11.4 | 6.3 | 12.0 | 19 | 12.0 | 6.6 | 11.0 |  | 8905 | Contact Force 12-17 gns. |
| 3/402AP | $2$ | $\begin{aligned} & 19 / 5 c 0 / 479 \\ & 18 / 5 c 0 / 479 \end{aligned}$ | $\begin{array}{r} 7 \\ 120 \end{array}$ | $\begin{array}{l\|l\|} 1 \\ 1+2 \end{array}$ | $\begin{array}{r} 460 \\ 88 \end{array}$ | 63 | 48 | 15 | 28 | 60 | 50 | 16 | 26 |  | 890W |  |
| 3/402AQ | $2$ | $\begin{aligned} & 30 / 500 / 479 \\ & 12 / 500 / 479 \end{aligned}$ | $\begin{array}{r} 20 \\ 1,700 \end{array}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 250 \\ 27 \end{array}$ |  |  | 63 | 78 10.3 |  |  | 66 | $\begin{array}{r} 74 \\ 9.8 \end{array}$ |  |  | Max. Contact Force 30 gms . |
| 3/402AR | $2$ | $\begin{aligned} & 27 / \mathrm{sco} / 479 \\ & 27 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 140 \\ & 140 \end{aligned}$ |  | 15 |  | 33 39 |  | 15.5 |  | $\begin{aligned} & 31 \\ & 37 \end{aligned}$ |  |  |  |
| 3/402AS | $2$ | $\begin{array}{r} 13 / \mathrm{sco} / 479 \\ 8 / \mathrm{sco} / 479 \end{array}$ | $\begin{array}{r} 3 \\ 1.8 \end{array}$ | $1+2$ | 330 |  | 39 |  | 90 |  | 41 |  | 85 |  |  |  |
| 3/402AU | $2$ | $\begin{aligned} & 33 / 500 / 479 \\ & 33 / 500 / 479 \end{aligned}$ | $\begin{gathered} 145 \\ 145 \end{gathered}$ | $1+2$ 2 | $\begin{aligned} & 45 \\ & 82 \end{aligned}$ |  |  | 9.5 | $\begin{aligned} & 12 \\ & 22 \end{aligned}$ |  |  | 10 | $\begin{array}{r} 11.4 \\ 21 \end{array}$ |  |  |  |
| 3/402AV | $2$ | $\begin{aligned} & 20 / 5 C 0 / 479 \\ & 13 / 5 C 0 / 479 \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 430 \\ & 550 \end{aligned}$ |  |  | 113 | $\begin{aligned} & 139 \\ & 212 \end{aligned}$ |  |  | 119 | $\begin{aligned} & 132 \\ & 202 \end{aligned}$ |  |  | Max. Contact Force 30 gris. |
| 3/402AW | $2$ | $\begin{aligned} & 34 / \mathrm{sco} / 479 \\ & 12 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{array}{r} 300 \\ 1,700 \end{array}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 55 \\ & 26 \end{aligned}$ |  |  | 14 | $\begin{aligned} & 18 \\ & 11 \end{aligned}$ |  |  | 15 | 17 10 |  |  |  |
| 3/402AX | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 3 / 5 C 0 / 479 \\ & 3 / 5 C 0 / 479 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | 1+2 | 50 |  |  | 10.4 | 12.8 |  |  | 11 | 12.2 |  |  |  |
| 3/402AY | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 20 / \mathrm{sco} / 479 \\ & 12 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{array}{r} 7 \\ 1,700 \end{array}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{array}{r} 430 \\ 26 \end{array}$ | 8.5 |  | 102 | 125 | 8 |  | 107 | 119 |  |  | Mär. Contact Force 30 gms. |
| 3/402AZ | $1 \begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 33 / \mathrm{ScO} / 479 \\ & 33 / \mathrm{sco} / 479 \end{aligned}$ | $\begin{aligned} & 145 \\ & 145 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1+2 \end{aligned}$ | $\begin{aligned} & 82 \\ & 41 \end{aligned}$ | 17 | 6.6 |  | 15 | 16 | 7.0 |  | 14 |  |  | Max. Break Contact Force 30 gms. |
| $3 / 402 \mathrm{AAB}$ | $3\left[\begin{array}{l} 1 \\ 2 \end{array}\right.$ | $\begin{aligned} & 6 / \mathrm{SCO} / 479 \\ & 7 / \mathrm{SCO} / 479 \end{aligned}$ | 75 50 | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & 120 \\ & 140 \end{aligned}$ | 28 | 20 |  | 58 | 27 | 21 |  | 55 |  |  | Max. Contact Force 30 gms. |
| 3/402AAC | $1 \begin{aligned} & 1 \\ & 2\end{aligned}$ | $\begin{aligned} & \text { A47901 } \\ & \text { A47901 } \end{aligned}$ | 400 400 | $1+2$ | 31 | 4.5 |  |  | 7.3 | 4.3 |  |  | 6.9 |  |  |  |

[^0]Page 9.


[^0]:    END.

